

Background of Full-W Divertor Activity

New ITER divertor strategy

- From MAC-12 (Oct. 2011) [ITER_D_6SR5F7]: "[...] for budgeting purposes, the MAC supports the DG recommendation to de-scope to a single divertor during construction and initial five years of operation".[...] "As to the specific choice of divertor, MAC recommends delaying the decision for up to two years."
- These recommendations were adopted by the ITER Council during its ninth meeting in Nov. 2011 so that IO started to investigate the possibility of beginning operation with a full-W armoured divertor.

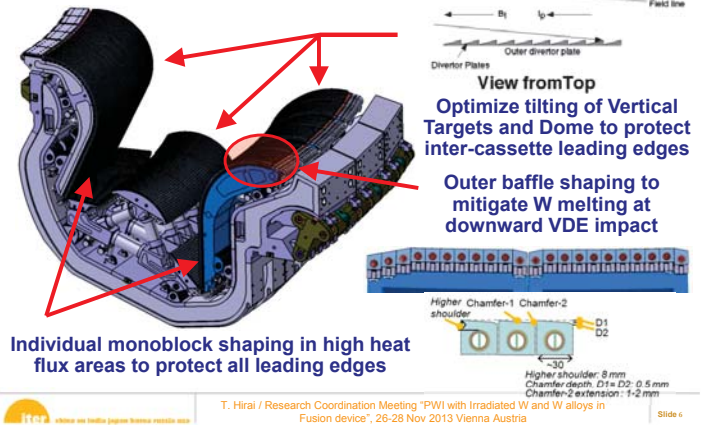
→ Tungsten Divertor Task Force was established to coordinate the design activity in IO and monitor the technology R&D in DAs

Schedule for full-W Divertor Implementation

- Final Design Review of Tungsten Divertor (26-28 June 2013) → close-out completed
 - ✓ Full-W Divertor design
 - ✓ Full-W Divertor technology qualification programme
- Physics Assessment → presented in STAC-14 and -15
 - ✓ Report from ITPA Topical Groups to STAC-14 (May 2013) giving physics/operational assessment on starting with a full-W divertor at ITER
 - ✓ JET misaligned lamella melt experiment
- STAC-15 (Oct 2013) recommended tungsten divertor as the first divertor
- ITER Council-13 (Nov 2013) endorsed the STAC recommendation on tungsten divertor as the first divertor
- Implementation of the decision into the baseline via a PCR (end-2013, SMP.0116.001032 milestone)

Full-W Divertor design: Main Features

Objective: minimum changes compared with the baseline (CFC/W) variant



Design Heat Flux and Number of Cycles

Input (ITER Research Plan)

- Available heating power during each ITER machine operation phase
- Scheduled number of pulses during each ITER machine operation phase from He-H through to DT operation

Assumption

- A full-W divertor, installed from the beginning of operations, should survive at least until the end of the first full DT campaign

Campaign	No. Pulses	Flattop success rate	$P_{H,max}$ (MW)	$E_{Sol,max}$ (MJ)	Pulses to 10 MWm ² (transient)	Pulses to 10 MWm ² (stationary)	Pulses to 20 MWm ² (transient)
H-He I	4200	0.8	60	58	0	0	0
H-He II	9800	0.9	60	58	450	0	0
DD	4950	0.9	73	68	1100	0	110
DT	5600	0.9	73	120	-	3700	180
Total	25000				1550	3700	290

Design Heat loads: 5000 cycles at 10 MW/m²; 300 cycles at 20 MW/m²

ITER Tungsten divertor and status

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Tungsten divertor Section, ITER Organization

On behalf of Tungsten Divertor Task Force at IO and all contributors

Disclaimer: The views and opinions expressed herein do not necessarily reflect those of the ITER Organization

T. Hirai / Research Coordination Meeting "PWI with Irradiated W and W alloys in Fusion device", 26-28 Nov 2013 Vienna Austria

W divertor development activity

Full-W divertor design development

- Extension of lifetime: update of the thermal loads specifications, nuclear aspects
- Introduction of W in the strike-point area (shaping aspects)
- Verification of the design via dedicated analysis

IO

Full-W Divertor qualification program (technology R&D)

Concerned DAs

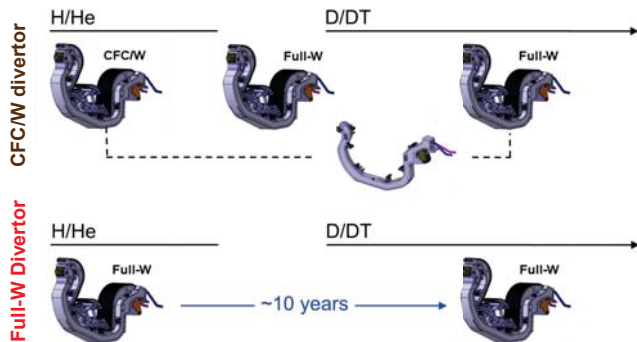
Assessment of the physics and operational risks of starting ITER with a full-W divertor

Physics community, ITPA, etc...

T. Hirai / Research Coordination Meeting "PWI with Irradiated W and W alloys in Fusion device", 26-28 Nov 2013 Vienna Austria

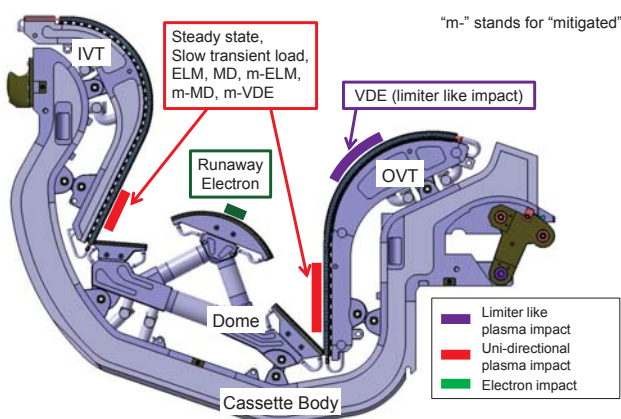
Divertor Maintenance strategy

Extension of Lifetime



T. Hirai / Research Coordination Meeting "PWI with Irradiated W and W alloys in Fusion device", 26-28 Nov 2013 Vienna Austria

Thermal Event Impact at Plasma-Facing Surfaces



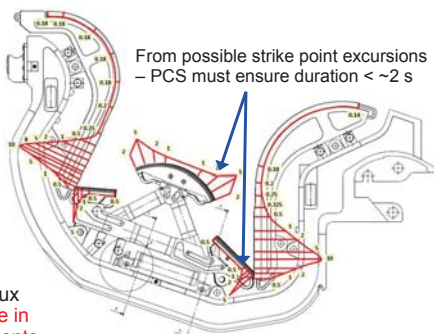
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Thermal loads specifications

Determination of thermal loads envelopes for design supporting analysis:

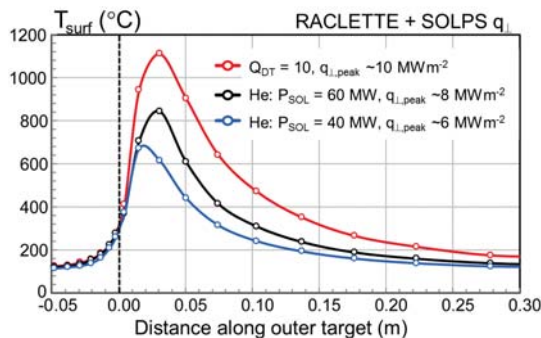
Plots of poloidal distribution for thermal analysis at highest steady performance ($Q_{DT} = 10$) → $q_{pk} = 10 \text{ MWm}^{-2}$



ASSUMPTION: these heat flux envelopes may simply double in magnitude during slow transients

(C9RF33)

Surface temperature: a key parameter



Calculation for 8 mm W monoblock (rectangular shape) armour thickness

(R. Pitts, PSI 2012)

Thermal loads specifications

"Fast transients" loads (event numbers and magnitude)

Vertical Displacement Events (VDE); Major Disruption (MD)

As for stationary loads, a thermal load specification was developed for VDE and MD: 4 main campaigns, two characteristic stored energies for each campaign; Mitigated and unmitigated

	VDE									
	Plasma stored energy (MJ)	No. of pulses	Flux top excursions above rate	Flux top excursions above rate	DW VDE rate	Unmitigated DW VDE rate (MJ/m²)	No. of mitigated DW VDE	Unmitigated DW VDE rate (MJ/m²)	No. of mitigated DW VDE	Unmitigated DW VDE rate (MJ/m²)
He-H I	30	4200	0.8	0.5	0.05	0.8	67	6 (2)	17	34
He-H II	90	9800	0.9	0.5	0.02	0.9	79	18 (7)	9	102
DD	150	4950	0.9	0.5	0.01	0.95	21	30 (12)	<2	169
Full Power DT $Q_{DT} = 10$	210	5600	0.9	0.5	0.01	0.99	12	43 (16)	<1	237
	350	5600	0.9	0.5	0.01	0.99	12	71 (27)	<1	395

	MD									
	Plasma stored energy (MJ)	No. of pulses	Flux top excursions above rate	Flux top excursions above rate	Major Disruption rate	Unmitigated MD rate (MJ/m²)	No. of mitigated MDs	Unmitigated MD rate (MJ/m²)	No. of mitigated MDs	Unmitigated MD rate (MJ/m²)
He-H I	30	4200	0.8	0.5	0.2	0.75	202	6 (2)	84	49 (19)
He-H II	90	9800	0.9	0.5	0.12	0.85	450	18 (7)	79	146 (56)
DD	150	4950	0.9	0.5	0.08	0.92	164	30 (12)	14	243 (93)
Full Power DT $Q_{DT} = 10$	210	5600	0.9	0.5	0.05	0.95	120	43 (16)	6	341 (130)
	350	5600	0.9	0.5	0.05	0.95	120	71 (27)	6	568 (216)

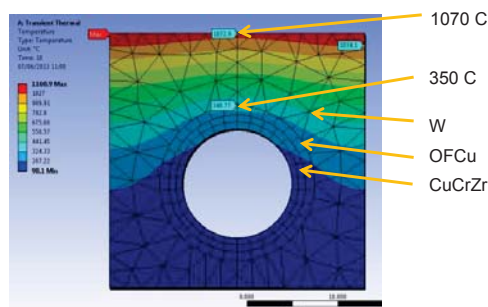
ELMs

Controlled ELMs spec for ITER: $\Delta W_{ELM}/A_{DIV} \leq 0.5 \text{ MJm}^{-2} \rightarrow \Delta W_{ELM} \sim 0.6 \text{ MJ}$ to avoid edge melting for unshaped (flat surface) monoblocks

(TGFMB6)

Temperature distribution in Monoblock

10 MW/m² steady state load



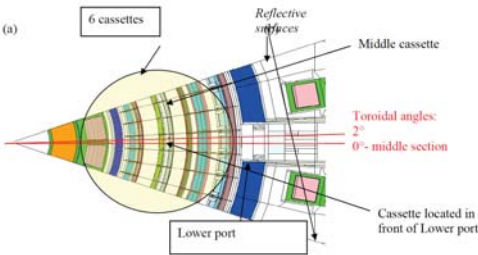
Calculation for 8 mm W monoblock (rectangular shape) armour thickness

Nuclear Analysis for ITER W Divertor

Model: with the latest ITER MCNP-5 Monte Carlo Code 3D model (MCNP ITER 40° model B-lite v-2)

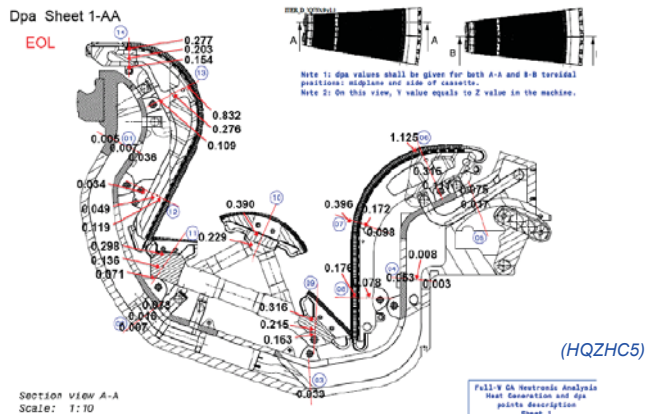
Assumption: 18% of the cumulated 3×10^{27} neutrons (ITER End of Life) during first divertor (up to end of the first full DT campaign)

Objective: Evaluate radiation damage, helium production and nuclear heating



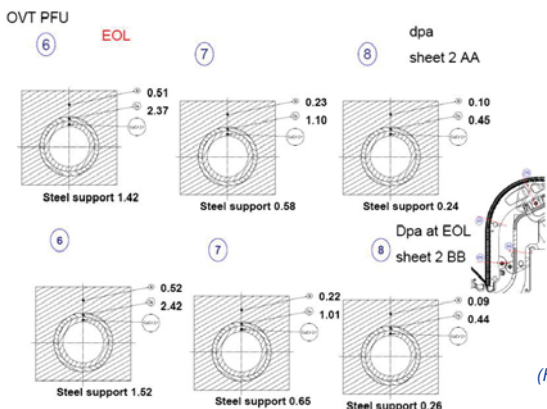
(HQZHC5)

Nuclear Analysis Results – DPA at End of Life



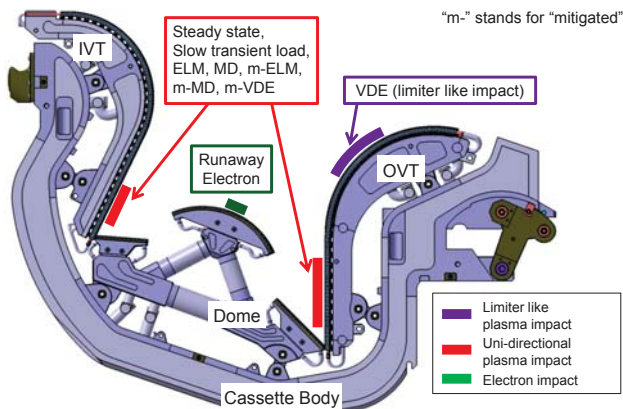
(HQZHC5)

Nuclear Analysis Results – DPA at End of Life



(HQZHC5)

Thermal Event Impact at Plasma-Facing Surfaces









"m-" stands for "mitigated"

Divertor Procurement Arrangement Status

Procurement Arrangements signed

5 are signed: 6 PAs allocated (in-kind contributions)

	PA17P-2A*	OVT	17 June 2009
	PA17P-2B	IVT	12 Mar 2010
	PA17P-2C	Dome	09 June 2009
	PA17P-2D	HHF Testing	23 Mar 2010
	PA17P-1A	CB+CA integration	08 May 2012
	PA17P-1B	Divertor Rails	Sept. 2014

1 to be signed:

(For rails: PCR290 implemented into baseline 27 Sept. 2010)

* To be renewed by Oct 2014 due to change to W divertor

W Material Specification (ITER_D_2EDZJ4v1.3)

1. Chemical composition (ASTM B760) : $\geq 99.94\%$

Element	Composition max, wt. %	Permissible variation in Check analysis, wt. %
C	0.01	± 0.002
O	0.01	+10% relative
N	0.01	+0.0005
Fe	0.01	+0.001
Ni	0.01	+0.001
Si	0.01	+0.001

2. Hardness HV30 (ASTM E92): ≥ 410

3. Density (ASTM B311): ≥ 19.0 g/cm³

4. Grain size at perpendicular to the rolling direction (ASTM E112) : 3 or finer

NDT: Visual Test and Ultrasonic Test

Requirement for the surface roughness: Ra < 6.3 μ m

Summary

- Showed: Divertor operation conditions: power and energy density (temperature) and dpa
- Appreciate: Assessment for machine operation conditions considering:
 - Fluctuation of power density and energy density (\rightarrow Fluctuation of temperature);
 - Temperature distribution in bulk W
 - Fluctuation of ΔT due to transient;
 - Fluctuation of particle flux
 - Helium and impurity flux,
 - Well-defined W material with engineering surface, i.e. Ra \sim 3.2 - 6.3 μ m
 - Shallow surface melting events, etc.
- Procurement of First W divertor had started. Procurement of second divertor will start before the first major shutdown